

APPLICATION NO. 09/826,118

TITLE OF INVENTION: Wavelet Multi-Resolution Waveforms

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Clean version of how the CLAIMS will read.

APPLICATION NO. 09/826,118

INVENTION: Multi-Resolution Waveforms

INVENTORS: Urbain Alfred von der Embse

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## CLAIMS

WHAT IS CLAIMED IS:

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Claim 1. (currently amended) An iterative eigenvalue least-squares LS method for designing digital mother Wavelets at baseband for multi-resolution waveforms and filters, said method comprising steps:

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power spectral density PSD representative requirements for said mother Wavelet  $\psi$  frequency  $\omega$  response  $\psi_{\omega}(\omega)$  in a multi-channel filter bank, specify

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- a) passband frequency range for waveform transmission,
- b) stopband spacing between adjacent filters,
- c) bounds on ripple over said passband,
- d) stopband filter attenuation,
- e) rolloff with frequency outside stopband,
- f) quadrature mirror filters QMF require the sum of said PSD's for contiguous filter responses to be flat over deadband which is said stopband,
- g) symbol-to-symbol interference ISI,
- h) adjacent channel interference ACI,

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said LS error metrics to measure said requirements (a)-(h) are derived as functions of said Wavelet  $\psi(n)$  assuming

30

- i) T and  $1/T$  are sample interval and sample rate equal to Nyquist sample rate,
- j)  $\psi$  is real and symmetric about  $n=0$ ,
- k)  $n = 0, +/-1, . . . , +/-ML/2$  digital index over said  $\psi$ ,
- l) M is interval between contiguous said  $\psi$ ,

m)  $1/MT$  is said  $\psi$  symbol rate and channel-to-channel separation,  
 n)  $L$  is length of said  $\psi$  in units of said  $M$ ,  
 said multiple-resolution properties require said LS metrics  
 5 to be constructed as functions of said Wavelet Fourier harmonics  $\psi_k(k)$  with  $k=0, +/-1, . . . , +/- (N_k-1)$  and  $N_k \geq L$  is a design parameter,  
 it is sufficient to use positive  $n=0,1, . . . , ML/2$  and  $k=0,1, . . . , N_k-1$  since said  $\psi(n)$  and  $\psi_k(k)$  are real and symmetric,  
 10  $ML/2+1 \times N_k$  matrix  $bw$  wherein "x" reads "by" maps  $\psi_k(k)$  into  $\psi(n)$  to within a scale factor by equations  

$$\psi(n) = \sum_k bw(n+1,k+1)\psi_k(k) \text{ for } n \geq 0, k \geq 0,$$

$$bw(n+1,k+1) = 1 \quad \text{for } n=0,$$

$$= 2 \cos(2\pi nk/ML) \text{ otherwise,}$$
 15 
$$= \text{row } n+1, \text{ column } k+1 \text{ element of } bw,$$
 said  $\psi(n)$  and  $\psi_k(k)$  are converted to column vectors by equations  

$$h = ML/2+1 \times 1 \text{ column vector of } \psi(n) \text{ with elements}$$

$$h(1) = \psi(n=0),$$

$$h(n+1) = 2\psi(n) \text{ for } n=1,2, . . . ML/2,$$
 20 
$$h_k = N_k \times 1 \text{ column vector of } \psi_k(k) \text{ with elements}$$

$$h_k(1) = \psi_k(k=0),$$

$$h_k(k+1) = 2\psi_k(k) \text{ for } k=1,2, . . . , N_k-1,$$
 said  $bw$  maps  $h_k$  into  $h$  to within a scale factor by matrix equation  

$$h = bw h_k,$$
 25 LS error metrics for band = passband, stopband, and QMF deadband requirements are derived as quadratic forms in said  $h$ ,  
 said LS error metrics are converted by said  $bw$  mapping into quadratic forms in said  $h_k$  equal to  $J(\text{band})=h_k' R h_k$  wherein said  $h_k'$  is the transpose of  $h_k$  and said  $R$  is a real square  
 30 symmetric matrix of LS errors in meeting said requirements.  
 LS ISI,ACI error metrics  $J(\text{ISI}), J(\text{ACI})$  are derived as non-linear

quadratic forms in  $h$  and converted by said  $bw$  matrix to the  
 non-linear quadratic form in  $h_k$  equal to  $J(ISI) = \delta E' \delta E$ ,  
 $J(ACI) = 2\delta E' \delta E$  wherein  $\delta E = AHh_k$  is a column vector and  
 matrix "A" in the matrix product  $AH$  is a function of said  $h$   
 5 hereby introducing said non-linearity, and said  $AH$  differ  
 for ISI and ACI error metrics,  
 LS cost function  $J$  is the weighted sum of said LS error metrics  

$$J = \sum w(\text{LS metric}) J(\text{LS metric})$$
 with summation over said LS metrics= passband, stopband,  
 10 QMF deadband, ISI, ACI with normalized weights  

$$\sum w(\text{LS metric}) = 1,$$
 said weights are free design parameters,  
 said iterative eigenvalue LS algorithm at each step finds the  
 optimum eigenvalue and eigenvector which minimize said  
 15 quadratic form  $J$  in  $h_k$  for a constant said "A",  
 said eigenvector is the optimum  $h_k$  which minimizes said  $J$  and  
 said  $bw$  equation derives the corresponding optimum  $h$  which  
 minimizes said  $J$ ,  
 step 1 in said iterative algorithm finds said optimum eigenvalue,  
 20 eigenvector,  $h_k$ ,  $h$  of  $J$  reduced by deleting said non-linear  
 ISI and ACI LS quadratic error metrics,  
 said  $h$  is used to evaluate said "A" matrices for step 2,  
 step 2 finds said optimum eigenvalue, eigenvector,  $h_k$ ,  $h$  for  
 minimum  $J$  using said "A" from step 1,  
 25 said  $h$  is used to evaluate said "A" for step 3,  
 steps 3,4, etc. continue until said minimum  $J$  converges to a  
 steady value and,  
 said optimum  $\psi_k(k)$  uses said  $bw$  to calculate optimum  $\psi(n)$  for  
 implementation as said Wavelet FIR digital waveform and  
 30 filter time response.

Claim 2. (currently amended) An LS method for designing digital mother Wavelets at baseband for multi-resolution waveforms and filters, said method comprising steps:

said PSD waveform representative requirements and assumptions

5 are recited in (a)-(n) in Claim 1,

said multiple-resolution properties require said LS metrics to be constructed as functions of said  $\psi_k(k)$ ,

said LS error metrics for said passband, stopband, and QMF deadband requirements are derived as squared vector norm functions of said  $h$  and converted by said  $bw$  matrix into

10  $J(\text{band}) = \|Bh_k\|^2$  wherein  $\|Bh_k\|$  is the vector norm of the column vector  $Bh_k$  and said  $B$  is the matrix of LS errors in meeting said requirements and wherein said squared vector norm is suitable for LS optimization,

15 LS ISI,ACI error metrics  $J(\text{ISI}), J(\text{ACI})$  are derived as squared vector norm functions equal to  $J(\text{ISI}) = \|\delta E\|^2$ ,  $J(\text{ACI}) = 2\|\delta E\|^2$  using said column vectors  $\delta E = AHh_k$  in claim 1,

LS cost function  $J$  is said weighted sum of said LS error metrics equal to  $J = \sum w(\text{LS metric}) J(\text{LS metric})$  defined in claim 1,

20 an LS gradient search algorithm finds optimum  $h_k(k)$  to minimize  $J$ ,

step 1 of said LS gradient search algorithm uses a Remez-exchange algorithm to find said optimum  $h_k(k)$  for said  $J$  reduced to said passband and stopband LS metrics,

25 step 2 uses the estimated  $h_k(k)$  from step 1 to initialize said gradient search,

step 3 selects one of several available gradient search algorithms, gradient search parameters, and stopping rules,

step 4 implements said algorithm, parameters, and stopping rule

30 selected in step 3 to derive said optimum  $h_k(k)$  to minimize  $J$  and,

said optimum  $h_k$  uses said  $bw$  to calculate optimum  $\psi(n)$  for

implementation as said Wavelet FIR digital waveform and filter time response.

5            Claim 3. (currently amended) Wherein said mother Wavelet in claims 1,2 generates multi-resolution dilated Wavelets, comprising steps and design: said Wavelet parameters are

- 10            a) scaling parameter  $p$  dilates sampling by factor  $2^p$  equivalent to sub-sampling by factor  $2^p$ ,
- b) translation parameter  $q$  translates said  $\psi$  by  $qM$  digital samples,
- c) frequency offset  $k$  is set by design,
- d) symbol repetition interval said  $M$  remains constant,
- 15            e) Wavelet length said  $L$  in units of said  $M$  remains constant,

step 1 uses said design harmonics  $\psi_k$  to generate said FIR time response  $\psi(n_p)$  at baseband with said bw equation

$$\psi(n_p) = \sum_k bw(n_p+1, k+1) \psi_k(k)$$

20            recited in claim 1 with

$$bw = 2 \cos(2\pi n_p k / ML) \text{ for } n_p > 0$$

wherein  $n_p = n / 2^p$  is  $n$  sub-sampled or equivalently dilated by the factor  $2^p$ ,

step 2 uses said  $\psi(n_p)$  to construct said multi-resolution

25            Wavelet  $\psi_{p,q,M,L,k}$  with equation

$$\psi_{p,q,M,L,k} = 2^{(-p/2)} \psi(n_p - qM) \exp(j2\pi kn_p / ML)$$

which is said FIR time response for parameters  $p, q, M, L, k$  wherein the subset  $p, M, L$  are the scale parameters,

design of said multi-resolution Wavelet includes

- 30            f) said  $T$  for  $n$  is increased to  $T2^p$  for  $n_p$ ,
- g) said  $1/T$  is reduced to  $1/T2^p$ ,
- h) said  $\psi$  symbol rate  $1/MT$  equal to said channel-to-channel separation is reduced to  $1/MT2^p$  in Hz and,

i) said  $\psi$  length  $(ML+1)T$  in seconds is stretched to  
 $(ML+1)T2^p$  in seconds.

5        Claim 4. (currently amended) Wherein said mother Wavelet in  
claims 1,2 generates multi-resolution constant sample rate  
dilated Wavelets, comprising steps and design:  
said Wavelet parameters are

a) said  $p$  dilates said  $\psi$  to increase said length from  
10         $ML+1$  to  $M_pL+1$  where  $M_p=M2^p$  is the dilated interval  
between contiguous  $\psi$ 's,

b) said  $q$  translates said  $\psi$  by  $qM_p$  digital samples,

c) said  $k$  is set by design,

d) said  $M_p=M2^p$  is dilated  $M$ ,

15        e) said  $L$  remains constant,

step 1 uses said design harmonics  $\psi_k$  to generate said FIR time  
response  $\psi(n_p)$  at baseband with said bw equation

$$\psi(n) = \sum_k bw(n+1, k+1) \psi_k(k)$$

recited in claim 1 with

20        
$$bw = 2 \cos(2\pi nk/M_pL) \text{ for } n>0,$$

step 2 uses said  $\psi(n)$  to construct said multi-resolution Wavelet  
 $\psi_{p,q,M,L,k}$  with equation

$$\psi_{p,q,M,L,k} = 2^{(-p/2)} \psi(n-qM_p) \exp(j2\pi kn/M_pL)$$

which is said FIR time response for parameters  $p,q,M,L,k$ ,

25        design of said multi-resolution Wavelet includes

f) said  $T$  remains constant,

g) said  $1/T$  remains constant,

h) said  $\psi$  symbol rate  $1/MT$  equal to said channel-to-channel  
separation is reduced to  $1/M_pT=1/MT2^p$  in Hz and,

30        i) said  $\psi$  length  $(ML+1)T$  in seconds is stretched to  
 $(ML2^{p+1})T$  in seconds.

Claim 5. (currently amended) Wherein said mother Wavelet in claims 1,2 generates multi-resolution up-sampled Wavelets, comprising steps and design:

said Wavelet parameters are

- 5 a) said p up-samples said digital sampling rate  $1/T$  to  $2^p/T$ ,
- b) said q translates said  $\psi$  by qM digital samples,
- c) said k is a design parameter,
- d) said M is constant
- e) said L is constant

10 step 1 uses said design harmonics  $h_f, \psi_k$  to generate said FIR time response  $\psi(n_p)$  at baseband with said equation

$$\psi(n_p) = \sum_k bw(n_p+1, k+1) \psi_k(k)$$

recited in claim 1 with

$$bw = 2 \cos(2\pi n_p k / ML) \text{ for } n_p > 0$$

15 wherein  $n_p$  is n up-sampled by the factor  $2^p$  and defined by equations

$$n_p = n_{\_p} + n 2^p$$

$$n_{\_p} = 0, 1, 2, \dots, 2^p - 1$$

20 wherein  $n_{\_p}$  is the index over the additional samples added to each sample n by said up-sampling,

step 2 uses said  $\psi(n_p)$  to construct said multi-resolution Wavelet  $\psi_{p,q,M,L,k}$  with equation

$$\psi_{p,q,M,L,k} = 2^{(-p/2)} \psi(n_p - qM) \exp(j2\pi k n_p / ML)$$

which is said FIR time response for parameters p,q,M,L,k,

25 design of said multi-resolution Wavelet includes

- f) said T is decreased to  $T/2^p$ ,
- g) said  $1/T$  is increased to  $2^p/T$ ,
- h) said  $\psi$  symbol rate  $1/MT$  equal to said channel-to-channel separation is increased to  $2^p/MT$  in Hz and,
- 30 i) said  $\psi$  length  $(ML+1)T$  in seconds is reduced to  $(ML+1)T/2^p$  in seconds.



Claim 6 (currently amended) Wherein said multi-resolution Wavelets in Claims 1-5 have properties comprising:

said scale parameters  $p, M, L$  and said design parameter  $1/T$  specify said multi-resolution Wavelets at baseband and said  $q, k$

5       specify time, frequency translations from baseband,

said design harmonics  $\psi_k(k)$  of mother Wavelet are said design coordinates for multi-resolution Wavelets,

said design harmonics  $\psi_k(k)$  use said bw matrix to generate said multi-resolution Wavelet baseband time response  $\psi(n)$  for

10       dilation, dilation of Wavelet length, and up-sampling as recited in Claims 3-5 and which is translated in time and frequency to said multi-resolution Wavelet  $\psi_{p,q,M,L,k}$ ,

said design harmonics  $\psi_k(k)$  are few in number compared to said  $\psi(n)$ ,

15       said  $\psi$  is designed to support a bandwidth-time product  $B_f T = 1 + \alpha$  with no zero excess bandwidth  $\alpha = 0$ ,

said multi-resolution Wavelets are designed to behave like an accordion in that at different scales said Wavelets are stretched and compressed versions of the mother Wavelet with

20       appropriate time and frequency translation,

said optimization techniques in claims 1,2 assume said  $\psi(n)$  symmetric about  $n=0$  and are applicable to other arrangements of  $\psi(n)$  with self-evident modifications,

optimization algorithms for finding said optimum set of  $\psi_k(k)$

25       use linear LS waveform and filter design methods recited in claims 1,2 and also use other methods and,

said linear waveform and filter LS design methods can be modified to design waveforms for applications including bandwidth efficient modulation BEM and synthetic aperture radar SAR.